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## INTENSELY RADIATING, SUPERCRITICAL SHOCK WAVES

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The quasisteady structure of strong, intensely radiating shock waves propagating at a velocity  $D$  in a gas with a density  $\rho_0$  and the laws of variation of their brightness temperatures  $T_\varepsilon$  with variation of  $D$  were investigated in [1, 2]. The role of emission is characterized by the parameter  $\eta = q_b/q_h$ , where  $q_b$  is the emission flux of a black body at the temperature  $T_s$  corresponding to the velocity  $D$  in accordance with the shock adiabat,  $q_h$  is the hydrodynamic flux of energy through the shock wave front, with  $q_b = \sigma T_s^4$ , while  $q_h = (1/2) \cdot \rho_0 D u_s^2$  ( $\sigma$  is the Stefan-Boltzmann constant and  $u_s$  is the gas velocity behind the shock wave front). Subcritical (in the terminology of [1, 2]) shock waves, i.e., those for which  $\eta < 1$ , are usually used as emission sources [3].

Only the soft part of the radiation emitted by the gas behind the front travels to large distances from the front. The hard part of this radiation is absorbed immediately ahead of the front, forming a heated layer. In [1-3], the value  $I_1$  of the first ionization potential of the working gas is taken as the arbitrary boundary  $\varepsilon_1$  separating the spectrum into these parts. We note that, according to calculations [4, 5] and measurements [6, 7] of the total emission flux,  $\varepsilon_1$  is 1-2 eV lower than  $I_1$  owing to absorption in broadened lines in the heated layer. As the velocity  $D$  of the front and the parameter  $\eta$  increase, the maximum temperature  $T_*$  ahead of the wave front grows. Absorption also begins in the long-wavelength part of the spectrum. Only quanta emitted in the heated layer itself emerge. The brightness temperatures  $T_\varepsilon$  and the thermal-radiation fluxes  $q_r$  at first follow  $T_s$  and  $q_b$  and then, having reached maxima, decrease [1-7].

In subcritical shock waves the highest values of  $q_r$  and  $T_\varepsilon$  can be obtained by using helium and neon, which have the highest values of  $I_1$ , as the working gases. In neon, for example, according to calculations [4, 5] and measurements [6-8], they reach 9-10 eV and 200-400 MW/cm<sup>2</sup> at velocities of 50-70 km/sec. Higher temperatures  $T_s$  can be attained when heavier gases are used. The equation of state for xenon [9], for example, can be approximated by the power function

$$e = AT^a \delta^{-\alpha}, \quad \delta = \rho/\rho_L, \quad (1)$$

where  $e$  is the internal energy per unit mass, kJ/g;  $\rho$  and  $\rho_L$  are the density and standard density of xenon (5.89 mg/cm<sup>3</sup>);  $A = 4.0$ ;  $a = 1.65$ ;  $\alpha = 0.14$  in the temperature range  $T = 2-30$  eV. Hence,

$$T_s = 0.35 u_s^{1.21} \delta_0^{0.085}, \quad \eta = 0.47 \cdot 10^{-2} u_s^{1.81} \delta_0^{-0.66}. \quad (2)$$

Here  $u_s$  is in km/sec;  $T_s$  is in eV;  $\delta_0 = \rho_0/\rho_L$ . At a velocity  $u_s = 40$  km/sec, according to (2), we obtain  $T_s = 30$  eV for  $\delta_0 = 1$  and the back-body emission flux  $q_b$  is 88 GW/cm<sup>2</sup>. In reality, however, shock waves are supercritical starting with  $u_s = 19$  km/sec and  $T_s = 13$  eV, while the maximum fluxes  $q_r^m$  are already reached for subcritical waves and, according to [6, 7] comprise 15-20 MW/cm<sup>2</sup>, corresponding to an effective temperature  $T_e = (q_r^m/\sigma)^{1/4} = 3.0-3.5$  eV. Thus, screening of the front prevents attaining high velocities and effective temperatures and obtaining large fluxes of radiation escaping from the front "to infinity."

The propagation of strong intensely radiating shock waves through a gas layer or cloud of limited size has been considered as one of the principles for weakening the screening effect [10-13]. After the front of the heated "tongue" arrives at the "boundary" between the cloud and the vacuum, radiation starts to escape almost freely. The flux density  $q_r$  of the emitted radiation proves to be of the order of magnitude of the hydrodynamic-flux density  $q_h$ , and hence  $T_e \sim u_s^{3/4} \delta_0^{1/4}$ . Thus, in principle,  $T_e$  and  $q_r$  as high as desired can be reached. For  $u_s = 40$  km/sec, e.g., we obtain  $q_r = 19$  GW/cm<sup>2</sup> and  $T_e = 21$  eV. With a decrease in the density  $\rho_0$  of the working gas it is easier to attain a given velocity  $D$ , but then the values of  $q_h$  and  $T_e$  decrease.

Let us estimate the characteristic thicknesses of the boundary layers. For supercritical shock waves, energy transfer in the heated layer has the character of radiative heat conduction [1, 2]. Neglecting effects of gas compression and motion in this layer, we write the energy balance for the quasisteady stage of the process of motion of the shock wave,

$$\rho_0 D e(T_s, \rho_0) = -(16/3) l_R(T_s, \rho_0) \sigma T^3 \partial T / \partial x,$$

where  $l_R$  is the Rosseland mean free path of the radiation. We approximate the dependence of  $l_R$  on  $T$  and  $\rho$  by the power function

$$l_R = B T^b \delta^{-\beta}. \quad (3)$$

For xenon,  $b = 1$ ,  $\beta = 1.7$ , and  $B = 1.8 \cdot 10^{-2}$  if  $l_R$  is in cm while  $T$  is in eV. Using (1), we obtain the temperature distribution in the heated layer:

$$T/T_s = (1 - x/x_T)^{1/\omega}, \quad \omega = 4 - a + b.$$

Thus, a thermal wave develops ahead of a hydrodynamic shock [2]. The thickness  $x_T$  of the layer is determined through the expression

$$x_T = \frac{16}{3\omega} \frac{\sigma T_s^4}{q_h} l_R^s = \frac{16}{3\omega} \eta l_R^s, \quad l_R^s = l_R(T_s, \rho_0).$$

Using Eq. (2), for xenon we have

$$x_T = 0.46 \cdot 10^{-4} u_s^{3.06} \delta_0^{-2.26}. \quad (4)$$

For  $u_s = 40$  km/sec and  $\delta_0 = 1$ , we find  $x_T = 3.6$  cm. The value of  $x_T$  grows rapidly with an increase in  $u_s$  and a decrease in  $\delta_0$ .

By using heavier gases than xenon, e.g., vapors of such metals as lead or bismuth, one can raise the temperature  $T_s$  and somewhat reduce the critical velocity  $u_s^*$  for which  $\eta = 1$ . Thus, for bismuth vapor at  $T = 2-30$  eV, the constants in Eqs. (1) and (3) are  $A = 2.04$ ,  $\alpha = 1.82$ ,  $\alpha = 0.125$ ,  $b = 1$ ,  $\beta = 1.79$ ,  $B = 0.83 \cdot 10^{-2}$ , and  $\rho_L = 9.39$  mg/cm<sup>3</sup>. Accordingly, instead of (2) and (4) we obtain

$$T_s = 0.54 u_s^{1.10} \delta_0^{0.069}, \quad \eta = 1.87 \cdot 10^{-2} u_s^{1.40} \delta_0^{0.72}, \\ x_T = 1.3 \cdot 10^{-4} u_s^{2.49} \delta_0^{-2.45}.$$

At low values of  $u_s$  (5-10 km/sec, let us say),  $T_s$  proves to be almost twice as high as for xenon. For  $\delta_0 = 1$ ,  $u_s^* = 17$  km/sec, while  $T_s^*$  is the same as for xenon, 12 eV. At  $u_s \approx 50$  km/sec, the difference in  $T_s$  almost disappears, which is connected with the faster growth in the degree of ionization  $\alpha_e$ , and hence in the quantity  $e$ , with temperature  $T$ .

At the same relative density  $\delta_0$ , the switch to heavier elements having higher atomic weights and greater standard densities  $\rho_L$  leads to an increase in the absolute density  $\rho_0$ , and with it to a rise in  $q_h$  for a given velocity  $u_s$ . The fluxes  $q_r$  and effective temperatures  $T_e$  grow correspondingly for supercritical waves. Thus, for bismuth vapor at  $u_s = 40$  km/sec and  $\delta_0 = 1$ ,  $q_h = 30$  GW/cm<sup>2</sup> and  $T_e = 23$  eV. Even so, in the regime of arrival of the radiating wave at the edge,  $T_e$  grows slower with an increase in  $D$  or  $u_s$  than does  $T_s$ , while  $q_r$  grows slower than  $q_b$ . This is connected with cooling of the gas behind the shock wave front when the radiation escapes freely. Temperatures close to  $T_s$  are maintained only in the region of optical depths of order  $1/\eta$ , and  $T \rightarrow T_e$  far from the front. We shall show how to avoid such cooling.

Let us assume that two shock waves are propagating toward each other. After the boundaries of the heated layers are joined, a gradual rise in the temperature and radiation fluxes, up to values of the order of  $T_s$  and  $q_b$ , begins in the plane of symmetry.

Let the gas layer behind the shock wave fronts be optically thick, while the heated gas ahead of the shock wave fronts is almost transparent. It is obvious that most of the radiation emitted by one front falls again on the front of the opposite wave, and vice versa. Cooling is absent. Such a situation (opacity of the gas behind a front and transparency of that ahead of it) can be provided, in principle, since  $\ell_R$  depends very strongly on  $\rho_0$ , while the compression behind the shock wave front is high (of the order of 10 in the absence of energy losses to emission and for an adiabatic index  $\gamma = 1.2$ ). Accordingly, the mean free paths are far greater ahead of a front than behind it at the same temperature (about 50-fold). We note that if the thickness  $x_S$  of the layer between the shock wave fronts is small (less than the steady-state thickness  $x_T$ ), then the wave structure differs from the quasi-steady-state structure. Under the condition that the gas is transparent or semitransparent, i.e., of the order of  $\ell_R^S$  for  $x_S$ , the radiative transfer differs in its character from radiative heat conduction.

Shock waves with high velocities can be generated by the gas streams of explosive [14, 15] or magnetoplasma [16] compressors, as well as by foils accelerated to high velocities by laser beams [17, 18], by electron or ion accelerators [19], by electromagnetic implosion [20], or by other means [13, 21]. In the process of such acceleration, rigid foils are usually vaporized and gradually expand, their density decreasing in comparison with the density of the solid, while their thermal energy is far lower than their kinetic energy. We shall assume that the shock wave is generated by a cool gas layer, having a density  $\rho_1$  higher than the density  $\rho_0$  of the working gas in which it is decelerated, traveling at a high velocity. Heat fluxes from the hot plasma behind the shock wave front also heat the "foil" itself. The foil must have a relatively large mass so that the radiation cannot leak out through it. This is also required so that the velocity of the shock wave does not decrease too much from its initial velocity through deceleration in the working gas.

To allow for all these factors, we made direct calculations of the corresponding non-steady radiative-gasdynamic problem. The calculation procedure is analogous to that used in [4, 5, 10-12]. It was assumed that at the initial time the shock waves were generated by the impact of two gas layers, of thickness  $\Delta x = 0.5x_0$  and density  $\rho_1 = 10\rho_0$ , on the working gas of thickness  $2x_0$  and density  $\rho_0$ . Thus, the mass  $m_1 = \rho_1\Delta x$  of the "foil" is five times greater than the mass  $m_0 = \rho_0x_0$  of the gas decelerating its flight, and therefore the motion takes place without a significant loss of velocity. It was assumed that both the decelerating working gas and the "foil" gas consist of bismuth, and that they are cool at the initial time, i.e., their temperatures are far lower than  $T_S$  corresponding to the initial ve-

locity  $u_0$  of the foil. A shock wave with an initial velocity  $D_0 = \frac{\gamma+1}{2} \frac{u_0}{1 + \sqrt{\rho_0/\rho_1}}$ , or with

$D_0 = 0.84u_0$  and  $u_S^0 = 0.76u_0$  for  $\gamma = 1.2$  and  $\rho_1/\rho_0 = 10$ , propagates in the working gas as a result of the decay of the discontinuity.

Let us consider variants with relative densities  $\delta_0 = 0.1$  and 1 for  $u_0 = 50$  km/sec, in which case the mass  $m_1$  of the foil is 6.6 and 66 mg/cm<sup>2</sup> while the initial kinetic energy is  $E_0 = 8.2$  and 82 kJ/cm<sup>2</sup>. The distributions of temperature  $T$  in the plasma at different times  $t$  are given in Fig. 1 (values of  $t$  in microseconds are indicated by the curves). For  $\delta_0 = 0.1$  (Fig. 1a), the temperature proves to be equalized over the entire gas ahead of the front practically at once, and it rises gradually with time to the value  $T_x = 34$  eV immediately before the reflection of the density jump. With an increase in  $\delta_0$  to 1 (Fig. 1b), the temperature rise at the center of symmetry occurs only after the arrival of the edge of the thermal wave, i.e., from the time  $t = 0.23$   $\mu$ sec.

In Fig. 2 we show the dependence on  $t$  of the unidirectional radiation flux densities  $q_S^-$  and  $q_S^+$  immediately ahead of the front in the heated layer, as well as the total flux density  $q_S = q_S^- - q_S^+$  at the front and the unidirectional flux density  $q_r$  at the center of symmetry for  $\delta_0 = 0.1$  (a) and  $\delta_0 = 1$  (b). The highest unidirectional flux density  $q_x$  (by the time  $t_x$  of reflection) for  $\delta_0 = 0.1$  is 13 GW/cm<sup>2</sup>, which is about twice as high as  $q_h$ . For  $\delta_0 = 1$ , it grows to 220 GW/cm<sup>2</sup>, which far exceeds both the hydrodynamic flux density  $q_h$  (four-fold) and the emission flux density  $q_b$  of a blackbody at  $T_S^0 = 29$  eV (2.8-fold). We note that, just as for  $\delta_0 = 0.1$ , the value of  $q_x$  can be increased by increasing  $\Delta x$  and  $x_0$  to values of the order of  $x_T$ .

If a small target is placed in the plane of symmetry, introducing a weak disturbance into the radiation field, the radiant flux incident on it will be close to  $q_r$ . The values

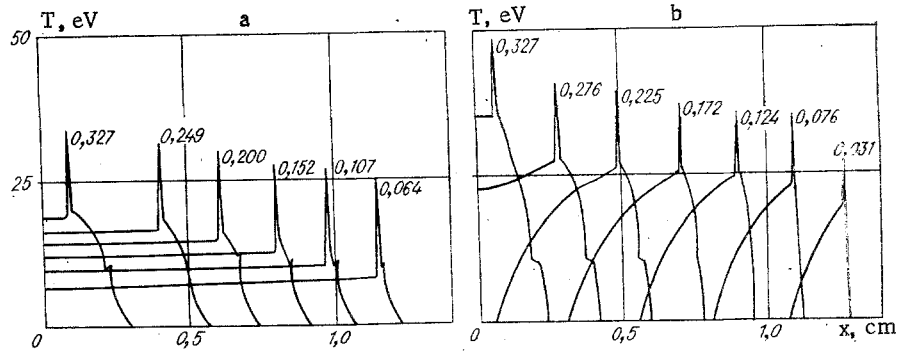


Fig. 1

of the energy  $E_r = \int_0^{t_x} q_r dt$  are 2.5 and 6.0 kJ/cm<sup>2</sup> for  $\delta_0 = 0.1$  and 1. Thus, the conversion factors are  $W = E_r/E_0 = 30$  and 7%. For  $\delta_0 = 0.03$  and 0.3,  $W = 2$  and 25%, respectively.

If the reflection of a shock wave from an obstacle located in its path occurs rather than the collision of equal shock waves, then after the edge of the heated layer approaches the obstacle, the heating of its surface layer, vaporization, dispersion of the vapor, and its further heating by the incident radiation begin. As the temperature of the vapor increases, it radiates toward the shock wave, which decreases the cooling of the gas behind it. The expanding vapor generates a shock wave, moving opposite to the main one, in the working gas. The collision of such waves leads to an additional temperature rise and an increase in the radiation flux at the obstacle. The radiation temperatures and fluxes reached, however, are lower than in a symmetric collision. Thus, for  $u_0 = 50$  km/sec and  $\delta_0 = 0.1$  we obtain  $q_x = 5$  GW/cm<sup>2</sup> and  $T_x = 28$  eV in the reflection. In this case, the characteristic pressure reached at the obstacle is already  $p_x = 0.9$  GPa before the reflection of the wave.

If we analyze the radiative transfer in the one-group approximation and assume that the power-law approximations (1) and (3) are acceptable, then we can employ similarity considerations. Conserving geometrical similarity, i.e., the ratio  $\Delta x/x_0$ , as well as the ratio  $\rho_1/\rho_0$  in the foil and in the decelerating gas, the degree of supercriticality of the shock wave at its initial velocity  $u_0$  (i.e., the value of the parameter  $\eta_0$ ) and the degree of transparency  $x_0/\lambda_R^0$  of the layer ahead of the wave, we can vary the density  $\rho_0$ , and with it the other parameters in accordance with the laws

$$\begin{aligned} u_0 &\sim \rho_0^{0.517}, x_0 \sim \rho_0^{-1.15}, q_x \sim \rho_0^{2.55}, E_0 \sim \rho_0^{0.68}, \\ m_1 &\sim m_0 \sim \rho_0^{-0.15}, t_x \sim \rho_0^{-1.67}, T_s^0 \sim \rho_0^{0.64}, p_x \sim \rho_0^{2.03} \end{aligned} \quad (5)$$

or

$$\begin{aligned} \rho_0 &\sim u_0^{1.93}, x_0 \sim u_0^{-2.22}, q_x \sim u_0^{4.93}, E_0 \sim u_0^{1.70}, \\ m_1 &\sim m_0 \sim u_0^{-0.29}, t_x \sim u_0^{-2.74}, T_s^0 \sim u_0^{1.24}, p_x \sim u_0^{3.93}. \end{aligned} \quad (6)$$

The ratio of the density  $\rho_{00}$  of the solid obstacle to the density  $\rho_0$  of the gas could have figured as one more similarity criterion. In the heating and dispersion of vapor in a regime of developed screening, however, when the flux density is not too high, the initial density  $\rho_{00}$  of the material is not an important parameter, since the vapor density is far lower than  $\rho_{00}$ .

Now let us consider shock waves converging toward a target of radius  $r_0$ . Let the gas behind their fronts be optically thick. If the gas between the shock-wave front of radius  $r_s$  and the target is, on the contrary, transparent, while the target is small ( $r_s \gg r_0$ ), then most of the radiation emitted by the front arrives again at other sections of it, while a given section is heated by radiation emitted from all the other sections (a "light reactor"). The role of absorption of radiation by the target is small if  $r_s^2 \gg r_0^2$ . Inside the front, the radiation flux density  $q_r$  is close to  $\sigma T_s^4$ , and for supercritical shock waves it can be far higher than  $q_h$ . The condition of transparency of the gas ahead of the front is not obligatory in order for the flux incident on the target to be greater than  $q_h$ . It is important that radiative heat conduction be sufficiently strong.

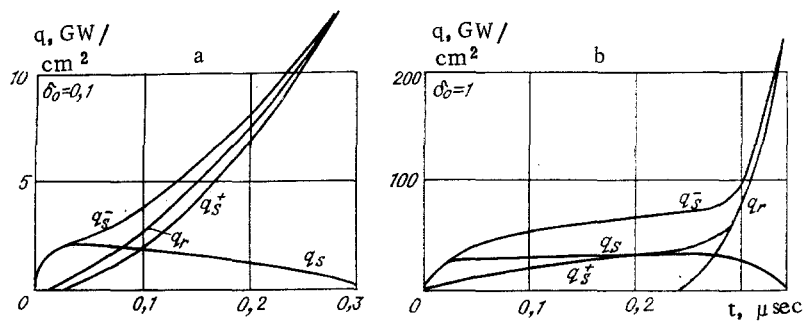


Fig. 2

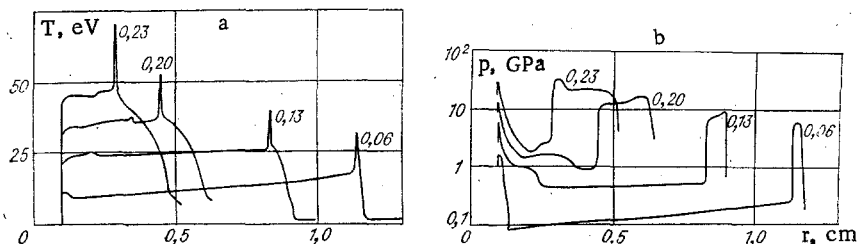


Fig. 3

The problem of the motion of a shell gathering toward the center and generating a converging shock wave, the gas ahead of which is transparent, has already been analyzed in [22] by estimates. A number of errors were committed in doing this. Thus, in determining the temperature of the gas in the region of its multiple ionization, expenditures on ionization were ignored and the adiabatic index  $\gamma$  was taken as  $5/3$ . In determining the degree of "transmission" of radiation back through the shell, the density in it was taken as equal to the initial density, whereas in reality it falls greatly as the heated material expands. On the other hand, in determining the mean free paths of radiation, the plasma of heavy elements was taken as hydrogenlike, and absorption and emission in lines were ignored. Finally, it was assumed that the photon gas is compressed adiabatically as the radius of the transparent "cavity" decreases, leading to an increase in the radiation temperature. It is easy to show, however, that under the analyzed conditions ( $\eta \leq 10-100$ ,  $u_s \leq 50-80$  km/sec), the energy and pressure of the radiation are small compared with the thermal energy and pressure of the matter (they are less than 1-10%). Nevertheless, all this cannot discredit the very idea of using converging shock waves to increase the radiation fluxes at the target. Moreover, the idea of a light reactor can also be used under the conditions of partial transparency of the gas ahead of the front. It is also necessary to allow for effects of reradiation by target vapor and the motion of the secondary shock wave generated by the vapor.

In numerical calculations allowing for all these factors, we assumed that the shock wave is generated by a spherical gas shell having an initial density  $\rho_1$  and velocity  $u_0$ , with an inner radius  $R_0$  and an outer radius  $R_1$ . Inside the shell, down to the target of radius  $r_0$ , the stationary and cool gas has a constant density  $\rho_0$ . We assumed that the target, the shell, and the working gas are bismuth vapor. We used calculated data on their optical properties [9], obtained with allowance for bound-bound transitions, the actual (not hydrogenlike) structure of the atoms and ions, and the absorption cross sections, using functions determined by the Dirac-Fock-Slater method.

We give the results of calculations for  $u_0 = 50$  km/sec with  $R_0 = 1.4$  cm,  $\Delta R = R_1 - R_0 = 0.2$  cm, and  $r_0 = 0.1$  cm. These values are close to those adopted in [22], with the exception of  $\rho_0$ , which is lower in our calculations, since the time of arrival of the radiation at the obstacle will be too small otherwise. For  $\rho_0 = 0.316 \cdot 10^{-2}$  g/cm<sup>3</sup> (or  $\delta_0 = 0.3$ ), the initial kinetic energy of the shell is  $E_k = 220$  kJ and the mass of the shell is  $M = 0.17$  g. In Fig. 3a, b we give the distributions over the radius  $r$  of the temperature  $T$  and pressure  $p$ , respectively, at different times  $t$  (the values of  $t$  in microseconds are given by the curves). The temperature ahead of the shock wave front gradually rises as it approaches the obstacle. The pressure at the vaporizing sphere, practically from the very start, proves to be close to the pressure at the front of the radiating shock wave and increases gradually with time. The

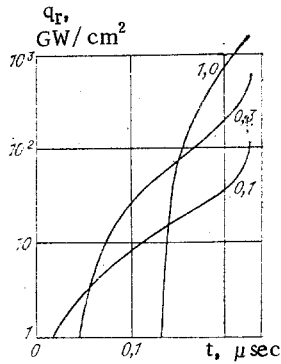


Fig. 4

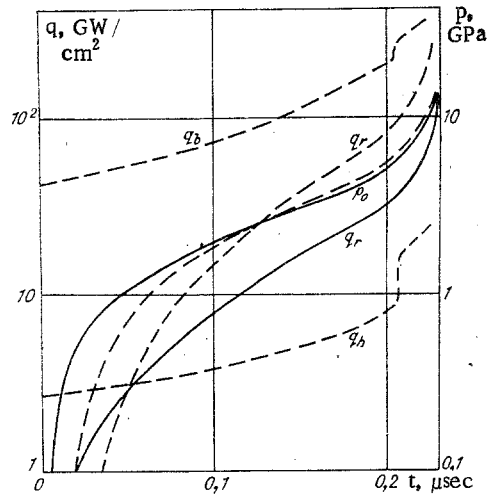


Fig. 5

radiation flux density  $q_x$  and the pressure  $p_x$  at the obstacle before the reflection of the shock wave are 210 GW/cm<sup>2</sup> and 14 GPa. For  $\delta_0 = 1$  they already reach 1.2 TW/cm<sup>2</sup> and 52 GPa. Such values are far lower than those derived in [22], but still demonstrate the great possibilities of the method under consideration. For  $\delta_0 = 0.1$ , the values of  $q_x$  and  $p_x$  decrease to 35 GW/cm<sup>2</sup> and 6 GPa, which is noticeably higher than in the plane case, like the temperature  $T_x$  (40 eV instead of 34 eV). This is connected with weak effects of hydrodynamic cumulation.

The duration of the stage of high pressures and radiation flux densities shortens with an increase in  $\delta_0$ . For  $\delta_0 = 1$  it is only about 30  $\mu$ sec (in Fig. 4 we show the time dependence of the flux to a sphere for different values of  $\delta_0$ , indicated by the curves). This is connected with the fact that for high  $\delta_0$  the thermal wave moving ahead of the shock wave does not reach the target for a relatively long time. For the value  $\delta_0 = 3$  adopted in [22], the corresponding time is shortened to about 2 nsec.

In Fig. 5 the solid lines are the results of a calculation of the variant with  $\delta_0 = 0.1$ , e.g., the values of the radiative flux density  $q_r$  incident on the target, the hydrodynamic energy-flux density  $q_h$ , the flux density  $q_b$  of the emission of a black body at the temperature  $T_s$ , and the pressure  $p_0$  on the obstacle; the dashed lines are the results of a calculation for sizes  $R_0$ ,  $R_1$ , and  $r_0$  exceeding those indicated above by a factor of five (the time scale is altered accordingly). The character of the time variation of the pressure and its maximum value itself remain unchanged in the two cases, despite some variation in the maximum flux.

To scale these variants to other densities in the spherical case, one can use the same equations, (5) and (6), as in the plane case. In this case, the total energy  $\mathcal{E}$  and the total mass  $M$  vary by the laws

$$\mathcal{E} \sim \rho_0^{-1.42} \sim u_0^{-2.74}, \quad M \sim \rho_0^{-2.45} \sim u_0^{-4.74}.$$

We note that the collision of the main shock wave with the secondary wave moving away from the target, leading to a spike of temperature and radiation flux, occurs at a rather large distance from the target (at a distance of the order of  $2r_0$  under these conditions). Effects of hydrodynamic cumulation are weakly manifested by this time. The velocities of the wave and the shell vary insignificantly, so that effects of instability of the shock wave front and the ablation front propagating through the shell are hardly felt at all significantly.

The light-reactor effect should occur in the case of spherical or cylindrical symmetry of the converging waves, or for colliding plane waves, or when the surface geometry of the waves is more complicated. One of the advantages of using the method of deceleration, in the gas surrounding the target, of a shell accelerated to a high velocity, under conditions of strong radiative heat transfer to the target, is not only the possibility of attaining record temperatures and radiation fluxes, but also the possibility of using the effect of smoothing out and increasing the degree of symmetry of target irradiation in comparison with the degree of symmetry of the shell itself [23].

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